

Spurious internal wave generation during data assimilation in eddy resolving ocean model simulations

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Abstract

Data assimilation (DA) combines observational data and the dynamical ocean model to forecast the ocean state in a matter that is not possible from either observations or models by themselves. However, when DA updates are unconstrained by the model equations, the updates act as a non-physical forcing term in the model and can disrupt the dynamical balance of the model. Following an update, the model undergoes an adjustment process to restore its dynamical balance, involving the generation of spurious near-inertial oscillations and other internal gravity waves. In this study, we investigate spurious internal waves generated following DA updates in an ocean forecast system. We find that the spurious waves are in a broad range of frequencies and propagate long distances from their generation sites in the form of low-mode internal waves. The depth-integrated, time-mean near-inertial kinetic energy in a simulation with DA is 72% higher than that of a corresponding forward simulation with the same surface wind forcing. The presence of these spurious near-inertial waves disrupts the ocean model energetics, and minimizing them is crucial for using the assimilative model simulations to study small scale/high-frequency ocean dynamics. We discuss a possible solution for minimizing the DA induced spurious waves by using longer Incremental Analysis Update periods.

Keywords: Data Assimilation, Near-inertial waves, Hybrid Coordinate Ocean Model

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1 **1. Introduction**

2 The Global Ocean Forecast System (GOFS), the U.S. Navy’s operational global ocean pre-
3 diction system, runs daily at US Navy production centers. The system offers the Fleet accurate
4 3-dimensional measurements of ocean temperature, salinity, and current structure as well as the lo-
5 cation of mesoscale oceanic eddies and fronts. The current operational version of GOFS, version
6 3.1 (Chassignet et al., 2009; Metzger et al., 2017), relies on the Hybrid Coordinate Ocean Model
7 (HYCOM) (Bleck, 2002; Chassignet et al., 2003) coupled with the Community Ice Code version
8 4 (CICE4) (Hunke & Lipscomb, 2008). Over time, GOFS has improved its predictive capabilities
9 for ocean circulation over a wide range of spatio-temporal scales. The assimilation of observational
10 data using the Navy Coupled Ocean Data Assimilation (NCODA) system, a three-dimensional vari-
11 ational DA technique, has significantly lowered the forecast errors of sub-tidal fields (Chassignet
12 et al., 2009; Cummings & Peak, 2014). These accomplishments of GOFS 3.1 have motivated the
13 Navy to develop GOFS 3.5 that includes tidal forcing in a higher resolution ocean model ($1/25^\circ$
14 HYCOM) (Metzger et al., 2020).

15 In the last decade, the non-assimilative, high-resolution, global HYCOM with tides has demon-
16 strated accurate representation of barotropic and internal tides compared to observations (Arbic et al.,
17 2010, 2012, 2018; Shriver et al., 2012; Buijsman et al., 2020; Arbic, 2022). The simultaneous in-
18 clusion of tidal and atmospheric forcing in HYCOM simulations has shown to produce a partially
19 resolved super-tidal internal gravity wave continuum (Müller et al., 2015; Savage et al., 2017a) and
20 a geographical distribution of non-phase-locked internal tides (Shriver et al., 2014; Buijsman et al.,
21 2017; Savage et al., 2017b) that agrees with inferences from altimetry (Nelson et al., 2019). It is
22 therefore expected that with the addition of data assimilation, high-resolution HYCOM simulations
23 with tides will be able to accurately predict the amplitudes and phases of the non-phase-locked in-
24 ternal tides. This would make the assimilative HYCOM an ideal candidate to be used as an internal
25 tide correction model for next generation altimeter missions with fine spatial resolutions such as the
26 Surface Water Ocean Topography (SWOT) mission (Morrow et al., 2019).

27 However, the current implementation of DA in the high-resolution HYCOM simulations is
28 not without drawbacks. As with many intermittent DA methods, the data-derived corrections in

29 NCODA are not constrained by the model equations. Hence, the analysis state may not always be
30 dynamically balanced. In such cases, the DA corrections act as a non-physical forcing term in the
31 model equations and cause initialization shocks in the analysis fields. These shocks are generated
32 when the model undergoes a process of adjustment to regain the lost dynamic balance. In order to
33 minimize these issues, the HYCOM-NCODA system uses a method called Incremental Analysis
34 Update (IAU) (originally developed for atmospheric general circulation models by Bloom et al.,
35 1996) that smoothly distributes the DA corrections to the model states over a specified time window
36 (3 hours in the operational system). However, a detailed investigation into the effectiveness of the
37 IAU in the HYCOM-NCODA system was never carried out.

38 In this paper, we show that, in the high-resolution HYCOM forecast system (GOFS 3.5), the
39 current implementation of IAU still introduces initialization shocks in the model output fields. Past
40 literature investigating the issue of DA induced model imbalances have focused on local (non-
41 propagating) noise and the impact of this noise on the representation of mesoscale eddies (Lange
42 et al., 2017; Waters et al., 2017; Pilo et al., 2018; Gasparin et al., 2021). We find that analyzing
43 the near-inertial frequency range in the model output fields reveals the presence of spurious internal
44 waves. The generation and propagation of spurious near-inertial waves in assimilative ocean model
45 simulations has never been explicitly investigated before, to the best of our knowledge. The presence
46 of these spurious waves that can propagate long distances from their generation sites can severely
47 impact the ocean energetics in the model and render the assimilative simulations much less useful
48 for studying small-scale or high-frequency ocean dynamics. We also examine a possible solution to
49 minimize the generation of spurious waves through the use of different IAU periods.

50 The layout of this paper is as follows. In section 2, we describe the model setup and the ana-
51 lytical methods we use in the paper. The results from our analyses of the global ocean model sim-
52 ulations are discussed in section 3. We use a global HYCOM simulation coupled with NCODA to
53 present the problem of model adjustment and characterize the spurious NIWs in the model output.
54 The assimilative simulation is compared against a forward simulation, run with the same forcing
55 over the same time period. In section 4, we analyze the impact of the duration of IAU period on
56 the generation of spurious NIWs using regional simulations of HYCOM. Finally, a summary and

57 discussion of our findings are presented in section 5.

58 **2. Model configuration and analysis methods**

59 *2.1. Ocean model simulations*

60 The two global HYCOM simulations - one with DA (EXPT 21.6 in HYCOM terminology), and
61 the other with no DA (EXPT 19.0), are run on a tri-polar grid at $1/25^\circ$ horizontal resolution (~ 3 km
62 in mid-latitudes) and 41 vertical layers. The DA in EXPT 21.6 is provided by the NCODA system
63 with a 24-hr assimilation window and 3-hr IAU period. NCODA uses the daily mean of a short-
64 term HYCOM forecast as a first guess (background fields) in a 3D variational (3DVAR) scheme and
65 assimilates available satellite altimeter observations, satellite and in-situ Sea Surface Temperature
66 (SST) as well as available temperature and salinity profiles from eXpendable BathyThermographs
67 (XBTs), Argo floats and moored buoys (Metzger et al., 2020). The daily mean forecast is used
68 to filter the majority of the tidal signals from the DA. The global simulations have realistic atmo-
69 spheric forcing from the Navy Global Environmental Model (NAVGEM) (Hogan et al., 2014) with
70 60 atmospheric levels over a height of 19 km and a horizontal resolution of 0.17° . The atmospheric
71 forcing is applied every 3 hours. HYCOM uses relative winds over the ocean surface to calculate
72 the surface wind stress. The tidal forcing in the simulations includes the M_2 , S_2 , K_1 , O_1 , and N_2
73 tidal constituents. The HYCOM simulations use a K -profile parameterization (KPP) scheme as the
74 subgrid scale vertical mixing model. In this paper, we diagnose the hourly model output data from
75 May 20, 2019 to June 19, 2019 (30 days). The non-DA (forward) simulation, EXPT 19.0, is a
76 twin of EXPT 21.6 with the DA turned off on April 1, 2019 (50 days before the analysis period),
77 providing enough time for the model to reach a steady state.

78 We also run HYCOM simulations in a regional configuration in the Gulf of Mexico varying
79 different model parameters (wind forcing, tidal forcing, IAU period), to study the spurious NIWs
80 in isolation from the wind-driven NIWs in the region, and test the effect of IAU period on the
81 generation of the spurious NIWs. The regional simulations are discussed in detail in Section 4.

82 2.2. Analysis methods

83 2.2.1. Rotary velocity spectra

84 The rotary spectra analysis is a technique to decompose a vector time series into clockwise
85 and counter-clockwise components. The separation of a velocity vector into oppositely rotating
86 components can reveal important aspects of the wave field at the specified frequencies (e.g., Yu
87 et al., 2019). The method has proven especially useful for investigating wind-generated inertial
88 motions, currents over abrupt topography, diurnal frequency continental shelf waves, and other
89 forms of narrow-band oscillatory flow (Gonella, 1972; Leaman & Sanford, 1975). In many cases,
90 one of the rotary components (typically, the clockwise component in the northern hemisphere and
91 counter-clockwise component in the southern hemisphere) dominates the currents so that we need
92 to deal with only one scalar quantity rather than two. For example, inertial oscillations rotate almost
93 entirely clockwise (counterclockwise) in the northern (southern) hemisphere so that the counter-
94 clockwise (clockwise) component may be ignored. The clockwise spectra are usually defined for
95 negative frequencies and counterclockwise spectra for positive frequencies (Thomson & Emery,
96 2014).

97 In our analysis, the rotary spectra are computed, following methods in Thomson & Emery
98 (2014), from model horizontal velocity vectors. We first compute the 1-dimensional discrete Fourier
99 transform of complex-valued velocity. The clockwise and counter-clockwise rotary spectra are
100 formed by the one-sided autospectra and the quadrature spectra, calculated by multiplying the
101 Fourier coefficients by their complex conjugates. The surface velocity rotary spectra are zonally
102 averaged over 0.5° latitude bins.

103 2.2.2. Near-inertial wave (NIW) energetics

104 The near-inertial fields are obtained from the model output using the filter method described
105 in Raja et al. (2022). The phase-locked tides are removed from the model output fields using a
106 harmonic analysis and a bandpass filter is applied with frequency limits $0.8f - 1/13.21$ h equator-
107 wards of 56° and $[0.8 - 1.2]f$ polewards of $\pm 56^\circ$. The frequency band is designed in such a way
108 that semidiurnal internal tides that are generated poleward of 56° and propagate equatorward are re-
109 moved. This allows us to capture NIWs that have propagated a large distance from their generation

110 sites.

111 We use the filtered near-inertial fields to calculate the near-inertial surface wind power input, W

112 as

$$W = \boldsymbol{\tau}' \cdot \mathbf{u}'(z = 0), \quad (1)$$

113 where $\boldsymbol{\tau}'$ is the near-inertial surface wind stress and $\mathbf{u}'(z = 0)$ is the horizontal baroclinic near-
114 inertial velocity vector at the surface.

115 The depth-integrated near-inertial kinetic energy, KE is calculated following Raja et al. (2022)

116 as

$$KE = \frac{1}{2} \rho_0 \int_{-H}^0 |\mathbf{u}'|^2 dz, \quad (2)$$

117 and the depth integrated NIW energy fluxes in the horizontal are calculated as

$$\mathbf{F}_H = \int_{-H}^0 p' \mathbf{u}' dz, \quad (3)$$

118 where H is the seafloor depth, ρ_0 is the reference density, and the near-inertial pressure perturbation,
119 p' , is computed using the density anomaly, ρ' , as in Nash et al. (2005).

120 The three-dimensional HYCOM fields are also decomposed into vertical normal modes (Kelly,
121 2016; Buijsman et al., 2020). We adopt the same modal decomposition diagnostics used in Raja
122 et al. (2022). The hydrostatic Sturm-Liouville equation is solved for non-equidistant HYCOM
123 layers using 30-day mean profiles of buoyancy frequency in each horizontal grid cell, to obtain the
124 velocity eigenfunctions. The horizontal velocity eigenfunctions, \mathcal{U}_n , are projected onto the vertical
125 profiles of the horizontal baroclinic velocities, u , at every time step to yield the modal amplitudes in
126 each horizontal grid cell, i.e.,

$$\hat{u}_n(t) = \frac{1}{H} \int_{-H}^0 \mathcal{U}_n(z) u(z, t) dz, \quad (4)$$

127 where \hat{u}_n is the modal amplitude of n th mode.

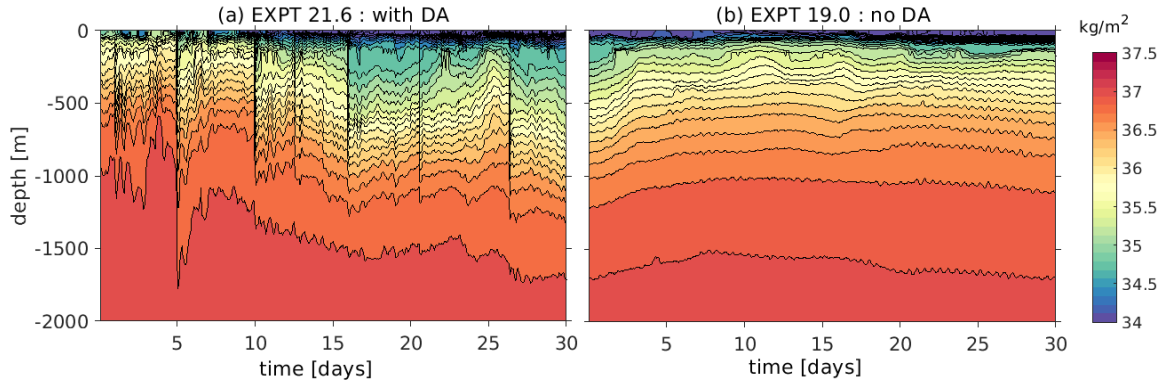


Figure 1: Time series of density contours for a vertical profile in the Gulfstream at 40.3° N, 302.5° W for (a) EXPT 21.6 (with DA) and (b) EXPT 19.0 (no DA). The time series is shown for the top 2000 m. The total seafloor depth at the location is 5162 m.

128 3. Spurious waves in global HYCOM simulations with DA

129 3.1. Model adjustment problem

130 During each DA cycle, the model variables are updated with corrections calculated by the DA
 131 system. The effect of these updates on the model output can be visualized using the time series
 132 of density contours from simulations with and without DA (Figures 1a and b, respectively). The
 133 density contours are shown at a location in the North Atlantic ocean (40.3° N, 302.5° W). We show
 134 the density contours for the upper 2000 m of the water column (the total depth at the location is
 135 5162 m). In Figure 1a, the insertion of corrections during DA causes shocks in the positioning of
 136 the isopycnals in the water column. The shocks are particularly severe on days corresponding to the
 137 availability of observational data (predominantly from satellite altimetry) at the location.

138 In addition to abrupt displacement of isopycnals, the insertion of corrections also forces the
 139 model out of its dynamic balance. We quantify the dynamic imbalance introduced by DA in the
 140 global ocean using the thermal wind relations, which can be written as (Vallis, 2017)

$$-f \frac{\partial v}{\partial p} + \frac{1}{\rho^2} \frac{\partial \rho}{\partial x} = R_x, \quad (5)$$

$$-f \frac{\partial u}{\partial p} - \frac{1}{\rho^2} \frac{\partial \rho}{\partial y} = R_y, \quad (6)$$

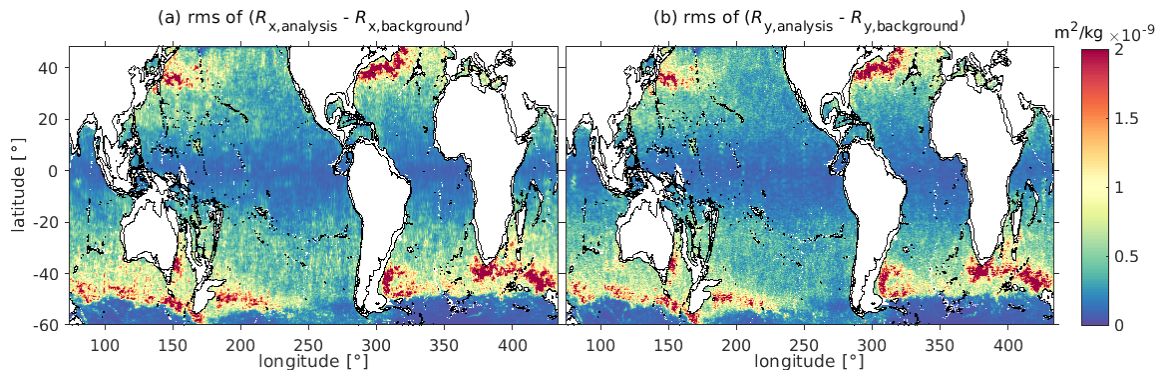


Figure 2: Root-mean-square of the depth integrated thermal wind imbalance generated during DA updates, calculated as (a) $R_{x,\text{analysis}} - R_{x,\text{background}}$, and (b) $R_{y,\text{analysis}} - R_{y,\text{background}}$ for 30 days in EXPT 21.6.

141 where u and v are the horizontal velocities, p is the pressure, ρ is the density, and f is the Coriolis
 142 frequency. The residual terms, R_x and R_y , in Equations 5 and 6 are the measures of thermal wind
 143 imbalance. We calculate the thermal wind imbalances of the background and analysis fields from
 144 NCODA, and evaluate the imbalance generated during the insertion of corrections as the difference
 145 of residuals of the background and analysis fields.

146 The root-mean-square of the depth-integrated imbalances generated during the insertion of cor-
 147 rections along the x and y axes are shown in Figure 2a and b, respectively. The imbalances are
 148 higher in the western boundary current regions and the Southern Ocean. These are regions of
 149 high mesoscale variability, where we expect frequent corrections to the model from the DA system
 150 (NCODA) in order to accurately capture the positions of the mesoscale eddies. Our finding implies
 151 that the geostrophic coupling within NCODA does not maintain the thermal wind balance very well.

152 The thermal wind balance does not apply near the equator because the Coriolis force goes to
 153 zero there. In the equatorial region, the dominant dynamic balance is between the ocean pressure
 154 gradients and the applied wind stress near the surface. The insertion of DA corrections can disrupt
 155 this balance near the equator, and trigger spurious vertical velocities and equatorial waves. Waters
 156 et al. (2017) discusses this type of model imbalance and proposes a modified bias pressure correction
 157 method to reduce the spurious vertical velocities near the equator. We focus on the DA induced
 158 dynamic imbalances that can lead to the generation of propagating near-inertial waves, away from

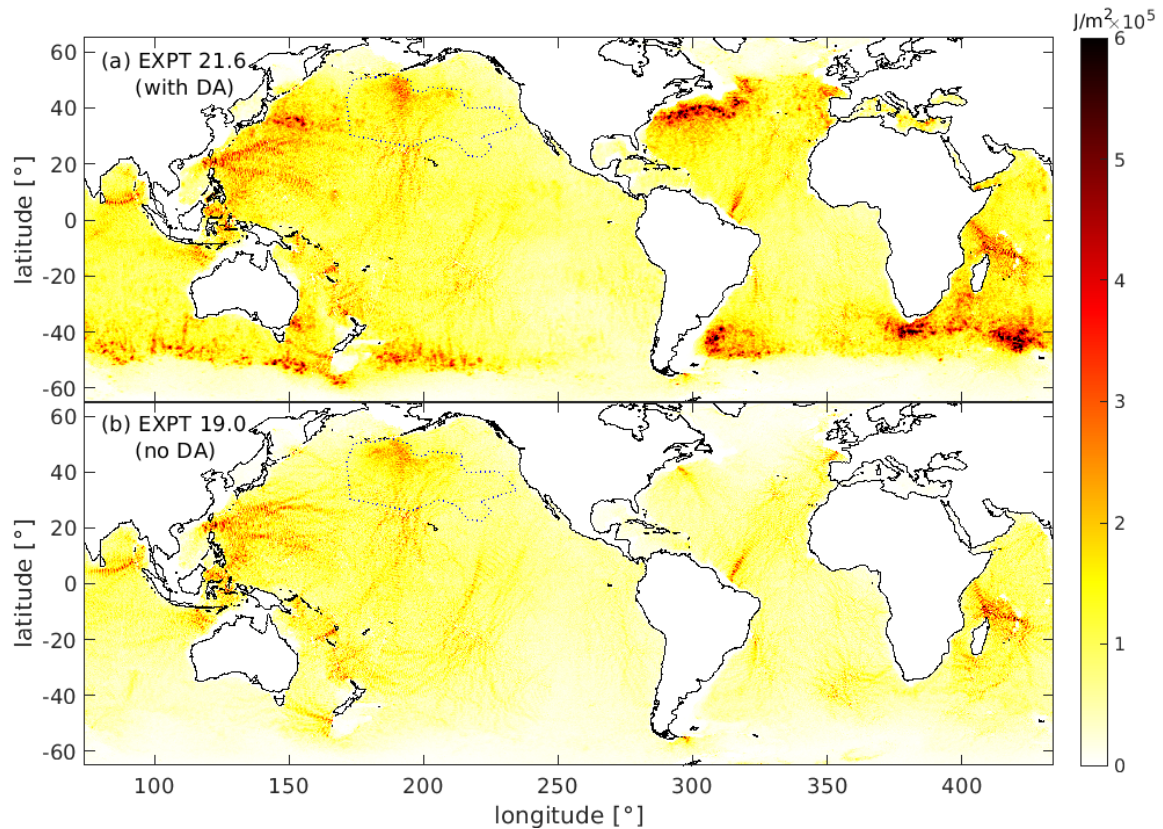


Figure 3: Root-mean-square ΔE_g in (a) EXPT 21.6 (with DA) and (b) EXPT 19.0 (No DA). The area enclosed by the blue dotted polygon is the region with TBI.

159 the equator.

160 The dynamic imbalance generated during the insertion of corrections is also associated with
 161 a change in the gravitational potential energy (E_g) of the water column when the depths of the
 162 isopycnals are adjusted by the DA correction. We evaluate the depth-integrated, volume averaged
 163 E_g following Butler et al. (2013) as $E_g = \int_{-H}^0 \rho g z dz$, where g is the acceleration due to gravity and
 164 H is the depth of the ocean floor. The change in E_g during the daily update in EXPT 21.6, ΔE_g , is
 165 calculated as the difference between E_g before and after the insertion of corrections in the model.
 166 We also compute ΔE_g in the forward simulation (EXPT 19.0) over the time duration corresponding
 167 to the update time in EXPT 21.6, for comparison.

168 The root-mean-square ΔE_g values for the simulation with and without DA are shown in Fig-

169 ures 3a and b, respectively. The regions with high ΔE_g in EXPT 21.6 correspond with the regions
170 with enhanced thermal wind imbalance, in particular the western boundary current regions and the
171 Southern Ocean (compare Figure 3a with Figure 2). The ΔE_g is also enhanced along many internal
172 tide beams in both simulations (Figures 3a and b). This enhanced ΔE_g is associated with the aliasing
173 of diurnal and semi-diurnal internal tides and the super-tidal internal gravity waves (e.g., see Figure
174 16 of Savage et al., 2017b). The values of ΔE_g are also elevated in the North Pacific in both simu-
175 lations. This might be due to thermobaric instability (TBI), a numerical instability in HYCOM, due
176 to imperfect compensation for compressibility in the pressure gradient term (Buijsman et al., 2016,
177 2020; Raja et al., 2022). The area identified to have TBI is enclosed by a blue dotted polygon in
178 Figure 3.

179 During the update, potential energy is injected into the ocean. This artificial source of energy
180 drives the model adjustment process to regain the dynamic balance. The process of adjustment may
181 involve the generation of spurious inertial oscillations and high-frequency internal gravity waves. In
182 order to understand the spurious motions generated during model adjustment in detail, we examine
183 the velocity rotary spectra in the simulations with and without DA.

184 The zonally averaged surface velocity rotary spectra as a function of frequency and latitude
185 for EXPT 21.6 and EXPT 19.0 are shown in Figure 4a and b, respectively. The spectra in both
186 simulations are characterized by high-energy peaks at low frequencies (< 0.5 cpd) and diurnal,
187 semidiurnal, and latitude-varying near-inertial frequencies. The difference in the spectral densities
188 between the two experiments is shown in Figure 4c. The simulation with DA (EXPT 21.6) has
189 more energy concentrated in the sub-tidal frequencies and the near-inertial frequencies, associated
190 with the DA induced corrections to the placement of mesoscale eddies and the spurious inertial
191 oscillations, respectively.

192 In Figures 4d and e, we present a depth profile of the velocity rotary spectra in the Gulfstream
193 region at 40.3° N, 302.5° W (at the same location of the density timeseries shown in Figure 1) for
194 EXPT 21.6 and EXPT 19.0, respectively. The spectra for both simulations show peaks of energy
195 at the sub-tidal frequencies, semidiurnal and near-inertial frequencies. The difference of the spec-
196 tra between the two experiments (Figure 4f) shows that the simulation with DA has more energy

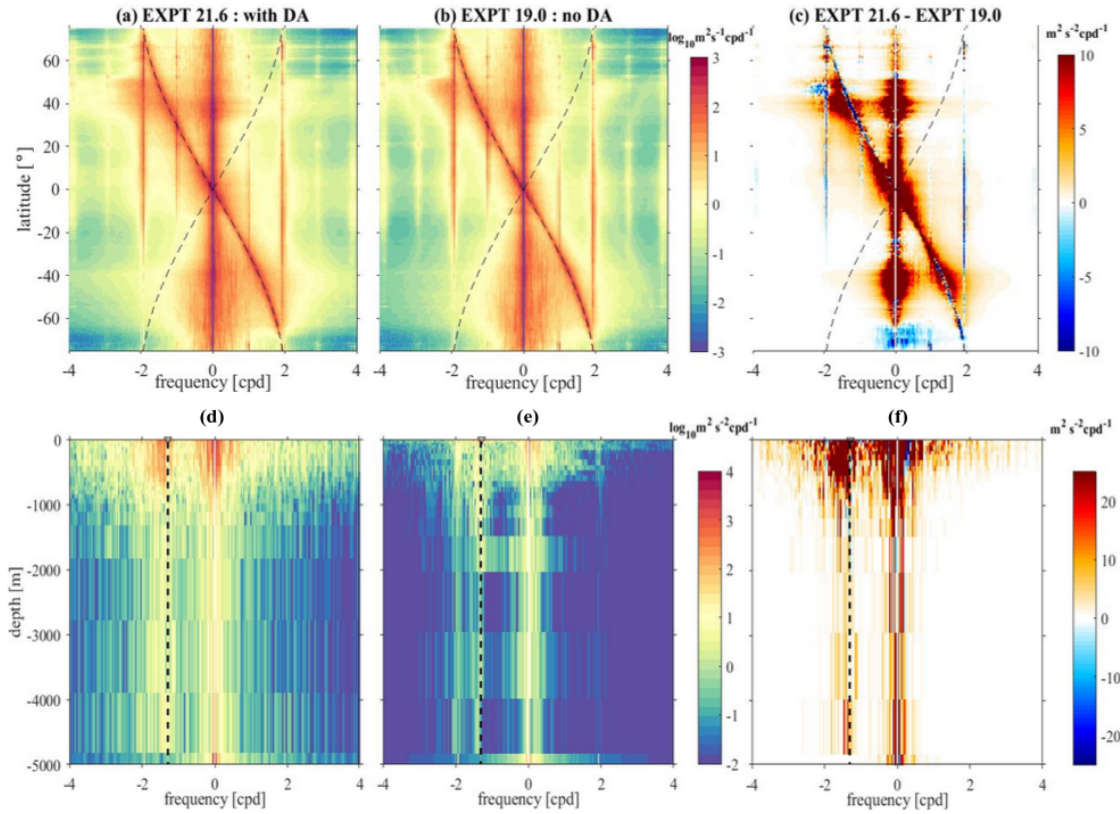


Figure 4: Zonally averaged surface velocity rotary spectra in (a) EXPT 21.6 (with DA) and (b) EXPT 19.0 (no DA). (c) The difference of spectral densities between EXPT 21.6 and EXPT 19.0. The dashed curves indicate the Coriolis frequency, f . Velocity rotary spectra with depth at 40.3° N, 302.5° W in the Gulfstream in (d) EXPT 21.6 and (e) EXPT 19.0. (f) The difference of spectral densities between EXPT 21.6 and EXPT 19.0. The black dashed line indicates the local Coriolis frequency, f .

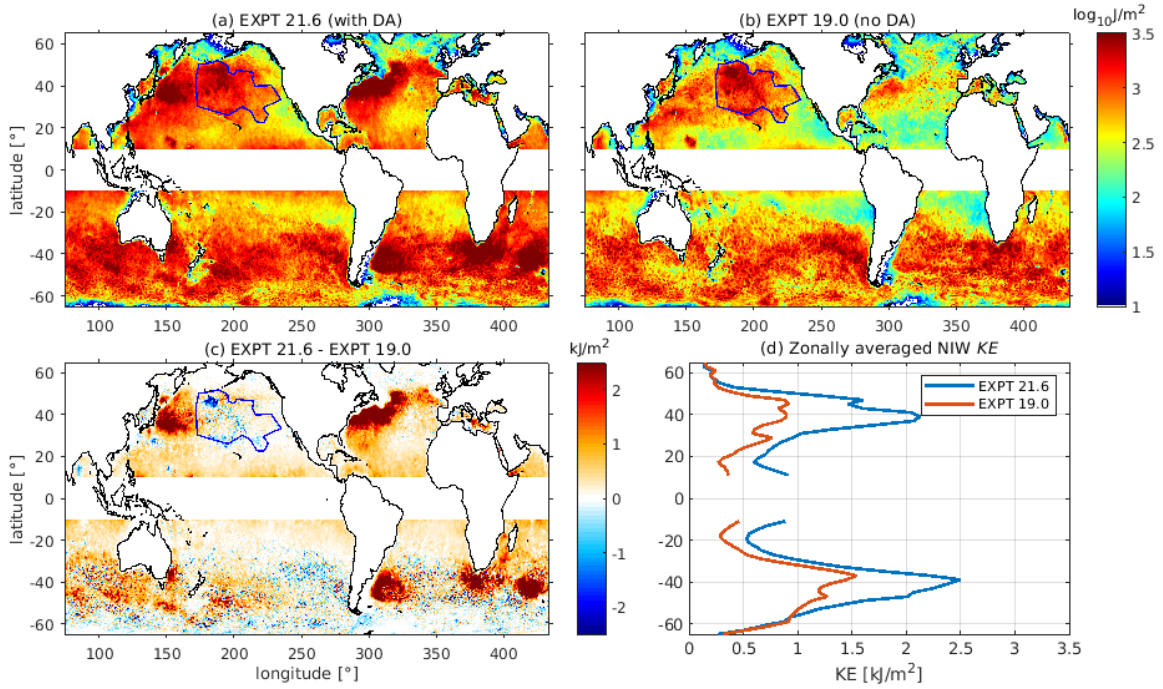


Figure 5: Depth-integrated, time-mean NIW kinetic energy (KE) for (a) EXPT 21.6 (with DA) and (b) EXPT 19.0 (no DA). (c) The difference of NIW KE between EXPT 21.6 and EXPT 19.0. (d) The zonally averaged NIW KE for EXPT 21.6 and EXPT 19.0. The area enclosed by the blue polygon are regions with TBI and are excluded from analysis.

197 concentrated in the sub-tidal and the near-inertial frequencies. Notably, the spurious near-inertial
 198 energy is present throughout the water column even though most of it is in the upper 1000 m.

199 3.2. Spurious near-inertial waves

200 The energy in the simulation with DA in the sub-tidal frequencies (seen in the rotary spectra in
 201 Figure 4) is associated with local processes that do not propagate horizontally from their generation
 202 sites. In contrast, the spurious energy in the near-inertial frequencies excites spurious near-inertial
 203 waves below the mixed layer that can propagate horizontally and mostly equatorward. We filter the
 204 model output fields in the near-inertial frequency range (as explained in Section 2.2.2) to analyze
 205 and characterize the spurious near-inertial motions in the assimilative simulation.

206 The depth-integrated, time-mean NIW kinetic energy for EXPT 21.6 (with DA) and EXPT
 207 19.0 (no DA) are shown in Figures 5a and b. Most of the NIW kinetic energy in both simulations

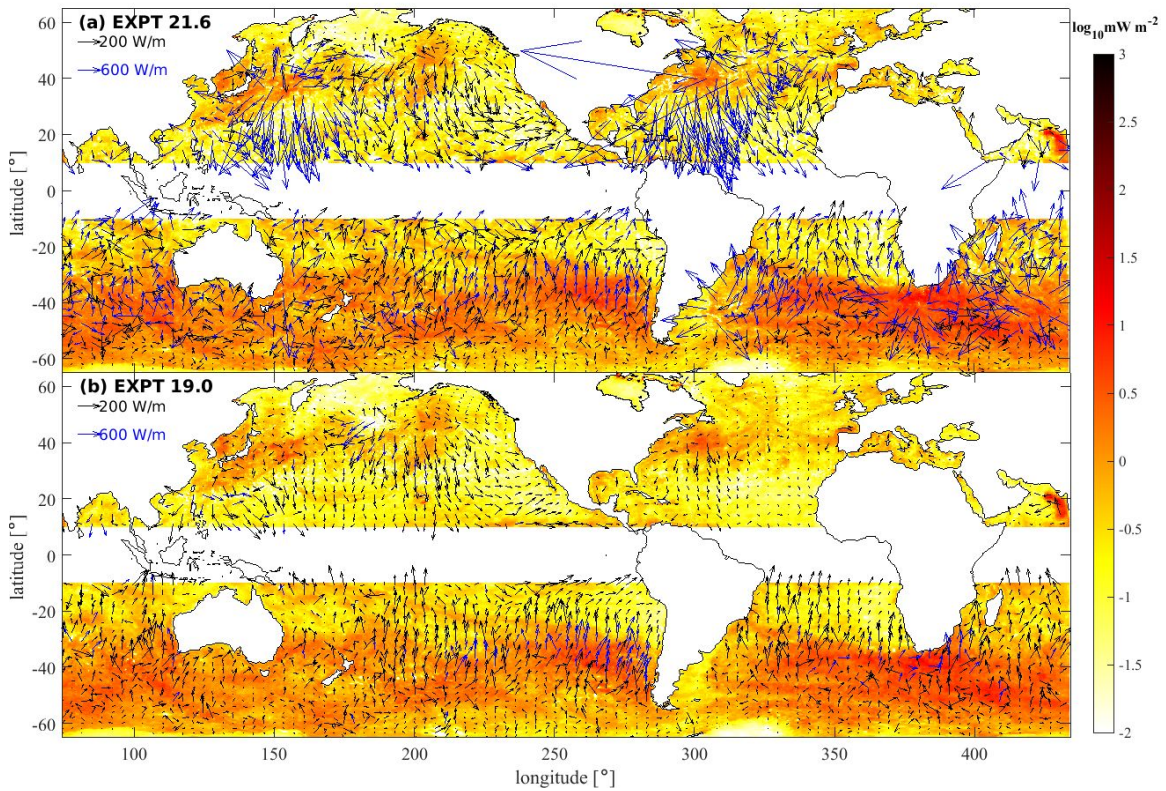


Figure 6: Time-mean near-inertial surface wind power input (W ; color), and depth-integrated NIW horizontal energy flux (vectors) for (a) EXPT 21.6 and (b) EXPT 19.0. The black vectors represent fluxes with a magnitude less than 100 W/m and the blue vectors represent fluxes with a magnitude larger than 100 W/m.

208 resides in the Southern ocean. There is also enhanced NIW kinetic energy in the western boundary
 209 current regions ($\sim 40^\circ\text{N}$) in both experiments. The difference of NIW kinetic energy between the
 210 simulation with and without DA (i.e., $KE_{\text{EXPT 21.6}} - KE_{\text{EXPT 19.0}}$) is shown in Figure 5c. EXPT 21.6
 211 has more NIW KE in most of the ocean in general, with particularly enhanced KE in the Southern
 212 ocean and western boundary current regions. The zonally averaged near-inertial kinetic energy for
 213 the 2 experiments is presented in Figure 5d. We find that with DA, EXPT 21.6 has 72% more NIW
 214 kinetic energy than EXPT 19.0, for the same wind forcing. EXPT 21.6 has higher energy in general
 215 throughout the global ocean but the energy is highest in regions with strong mesoscale variability.
 216 In these regions, the amplitude of the DA increments is large in order to correctly position the
 217 mesoscale features in the analysis fields (Figures 2 and 3).

218 In order to understand the horizontal propagation of NIWs in the simulations with and without
219 DA, we evaluate the horizontal energy fluxes as described in Section 2.2.2. The depth-integrated,
220 time-mean NIW horizontal energy fluxes (\mathbf{F}_H) for EXPT 21.6 (with DA) and EXPT 19.0 (No DA)
221 are presented in Figures 6a and b (vectors), respectively. The time-mean near-inertial wind power
222 input is shown in color in both figures. In Figure 6a (EXPT 21.6), strong near-inertial fluxes are
223 generated in regions with high mesoscale activity, particularly in the western boundary current re-
224 gions. The generated fluxes occur in all directions, including poleward, indicating that these fluxes
225 are due to waves with super-inertial frequencies. In Figure 6b (EXPT 19.0), near-inertial fluxes are
226 directed towards the equator from regions of high wind input in both hemispheres. The NIW energy
227 fluxes are the strongest in the southeast Pacific (around 500 W/m) and the Southern Ocean (around
228 300 W/m) where the wind input is large. Strong northward and diverging fluxes occur in the north-
229 ern Pacific south of the Aleutian islands in Figure 6a and b without any corresponding wind power
230 input. These fluxes might be due to TBI, as discussed in Buijsman et al. (2020). The broad-band
231 disturbances associated with the TBI also have super-inertial frequencies that allow for poleward
232 propagation.

233 The spurious NIW fluxes in the assimilative simulation propagate long distances equatorward
234 from their generation sites in the extra-tropics. What modal structures do these waves have in order
235 to persist such long journey without dissipation? In order to answer this question, we decompose
236 the baroclinic fields into vertical normal modes. The horizontal resolution of our model ($1/25^\circ$; 4
237 km near the equator) allows the first 5 semi-diurnal and near-inertial vertical modes to be resolved
238 in most of the ocean (Buijsman et al., 2020; Raja et al., 2022).

239 The zonally averaged rotary spectra computed from the modal amplitudes of horizontal baro-
240 clinic velocity (Equation 4) for the simulation with DA, without DA, and their difference are shown
241 in Figure 7. The difference of rotary spectra of the two experiments shows that the spurious near-
242 inertial energy mostly projects on mode 1 (Figure 7c). The results presented in Raja et al. (2022)
243 show that the mode 1 NIWs propagate with group speeds close to 1 m/s and reach distances of
244 ~ 1500 km from their generation sites before they dissipate. Therefore, the spurious NIWs gener-
245 ated in the simulation with DA persist for a long time and propagate long distances horizontally.

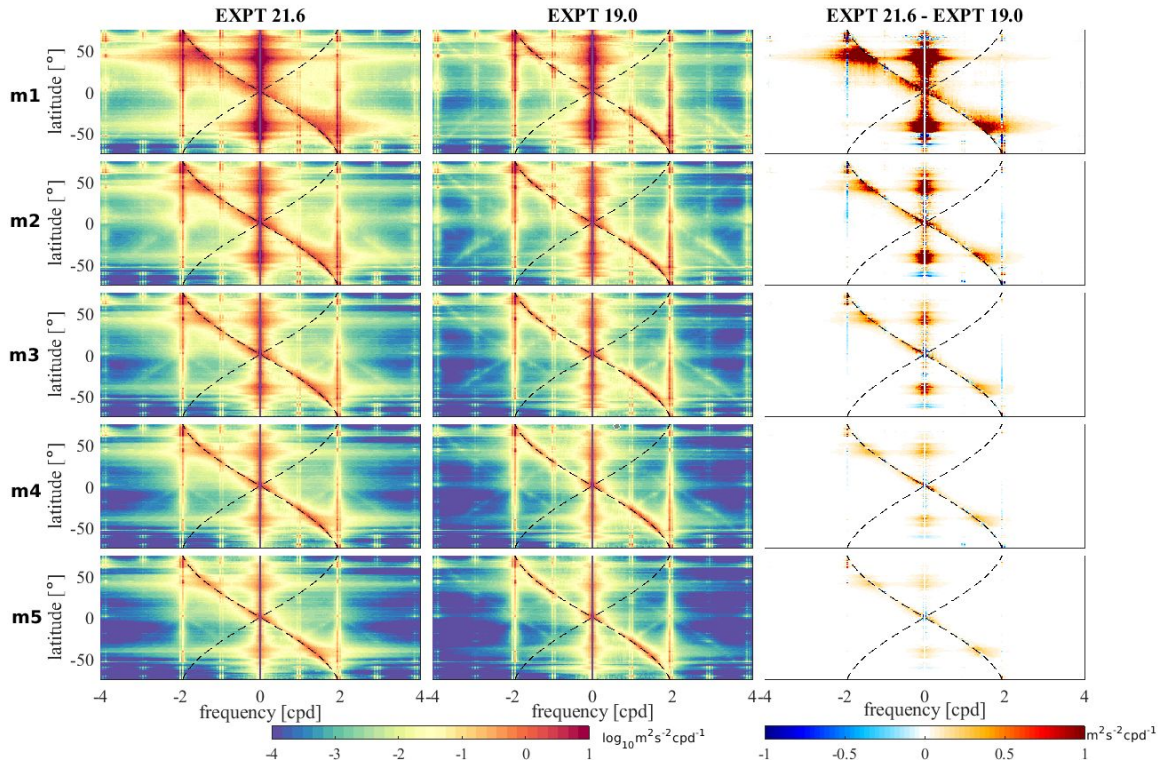


Figure 7: Zonally averaged velocity rotary spectra of modal amplitudes for modes 1 to 5 for EXPT 21.6 (first column), EXPT 19.0 (second column), and their differences (third column).

EXPT	Assimilation (T_{IAU} , if any)	Tidal forcing	Wind forcing
20.1	No DA	No	No
02.5a	TSIS (6 hr)	No	No
02.5b	TSIS (12 hr)	No	No
02.5c	TSIS (18 hr)	No	No
02.6	TSIS (24 hr)	No	No
20.0	No DA	Yes	Yes
02.0	TSIS (6 hr)	Yes	Yes
02.3	TSIS (12 hr)	Yes	Yes
02.7	TSIS (18 hr)	Yes	Yes
02.8	TSIS (24 hr)	Yes	Yes

Table 1: List of the regional HYCOM simulations of the Gulf of Mexico.

246 These propagating spurious NIWs may also interact with other small-scale, high-frequency motions
247 and affect the energetics throughout the ocean basin.

248 **4. A possible solution to spurious NIW generation due to DA**

249 In this section, we analyze the role of the IAU period in suppressing the generation of spurious
250 NIWs during DA. Bloom et al. (1996) introduced the IAU method as an initialization procedure
251 to minimize the excitation of inertial motions during DA updates. Using a linear analysis of the
252 IAU procedure, Bloom et al. (1996) demonstrate that it has the desired property of a low-pass time
253 filter on the analysis fields following an update. The IAU procedure filters out the spurious motions
254 with time periods less than the IAU period. In our analyses of the global simulation with DA,
255 where the IAU period is 3 hours, we find spurious near-inertial waves, which have time periods > 3
256 hours in the global ocean, generated following the DA update. This implies that 3-hr IAU is too
257 short to prevent the generation of spurious high-frequency motions. Hence, we evaluate simulations
258 with longer IAU periods to estimate the optimum IAU period for suppressing spurious NIWs in the
259 analysis fields.

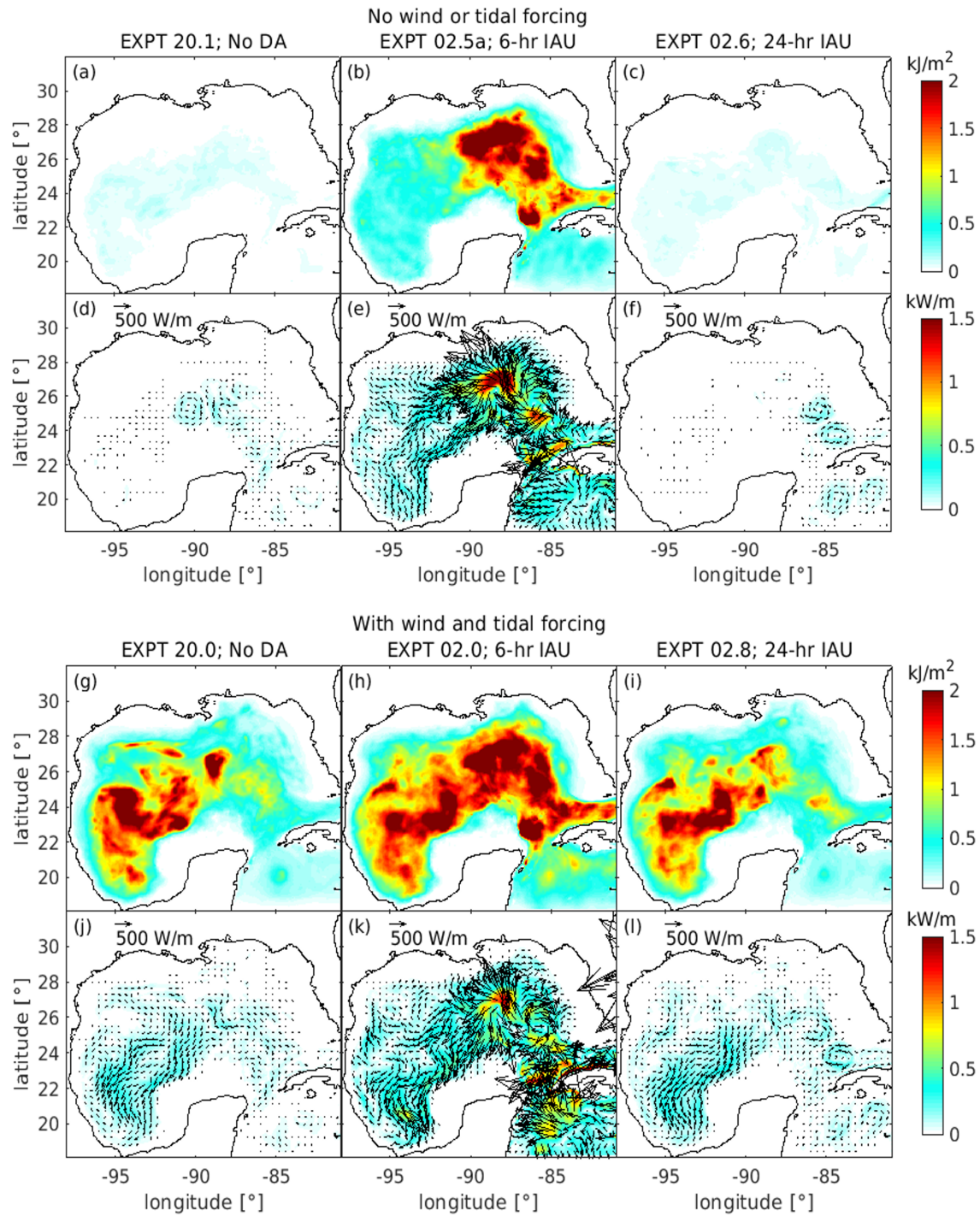


Figure 8: The depth-integrated, time-mean NIW kinetic energy in the Gulf of Mexico in simulations without wind and tidal forcing with (a) no DA, (b) 6-hr IAU, and (c) 24-hr IAU. The depth-integrated, time-mean NIW horizontal energy fluxes (vectors) and NIW flux amplitudes (color) in simulations without wind and tidal forcing with (d) no DA, (e) 6-hr IAU, and (f) 24-hr IAU. (g-l) are the same as (a-f), but for the addition of wind and tidal forcing.

260 In order to study the role of the IAU period in the generation of spurious NIWs, we establish
261 a test-bed using HYCOM simulations in an existing regional configuration of the Gulf of Mexico
262 (Dukhovskoy et al., 2015). The Gulf of Mexico region is also chosen because it has relatively weak
263 internal tides, strong surface winds and a dynamic mesoscale field. The simulations are run with
264 $1/25^\circ$ horizontal spatial resolution and 41 vertical layers, similar to the global model simulations.
265 Since the Navy’s NCODA system is proprietary and not publicly available, we use the open-source
266 data assimilation package, Tentral Statistical Interpolation System (T-SIS), developed by Srinivasan
267 et al. (2022), to assimilate observational data in the regional model as in Dukhovskoy et al. (2023).
268 The regional simulations have realistic atmospheric forcing from the Climate Forecast System Ver-
269 sion 2 (CFSv2), developed by the National Centers for Environmental Prediction (NCEP) (Saha
270 et al., 2014), with 0.205° horizontal resolution and hourly forcing frequency.

271 We first analyze the spurious NIWs in isolation from the physical internal waves in the region
272 by running an assimilative simulation without the wind and tidal forcing. We then test different IAU
273 periods and estimate the IAU period for which all the spurious NIWs are diminished in the model
274 output fields. The assimilative simulations are compared against a parallel forward simulation. The
275 same set of simulations are done with wind and tidal forcings to verify that different IAU periods
276 still leave the physical internal waves intact. We test IAU periods of 6, 12, 18 and 24 hours. The list
277 of regional simulations and their descriptions are shown in Table 1.

278 The time-mean, depth-integrated NIW kinetic energy and NIW energy fluxes for simulations
279 without wind and tidal forcing are shown in Figure 8a-f. The forward simulation without DA (Fig-
280 ures 8a and d) shows no presence of near-inertial motions. When the IAU period is 6 hours (Figures
281 8b and e), the DA generates spurious waves in broad near-inertial frequency band that diverge from
282 a region south of the Mississippi coast. When the IAU period is increased to 24 hours (Figures 8c
283 and f), the kinetic energy associated with the spurious NIWs is greatly diminished.

284 Figures 8g-i show the time-mean, depth-integrated NIW kinetic energy and NIW energy fluxes
285 for simulations with wind and tidal forcing. This time in the forward simulation (Figures 8g and j),
286 the wind-generated NIWs are present in the western Gulf of Mexico. In the assimilative simulation
287 with 6-hr IAU period (Figures 8h and k), the spurious NIWs present mostly in the eastern Gulf of

288 Mexico dominate the wind-generated NIWs. These spurious NIWs are due to large DA corrections
289 in the loop current region. When the IAU period is increased to 24 hours, the spurious NIWs are
290 minimal, and the NIW kinetic energy and fluxes in Figures 8i and l compare well with those of the
291 forward simulation (Figures 8g and j).

292 Figure 9a summarizes the depth and area integrated NIW kinetic energy in the Gulf of Mexico
293 for all the regional simulations listed in Table 1. In the experiments with and without wind and tidal
294 forcing, the NIW kinetic energy decreases with increasing IAU period, and the simulations with
295 24-hr IAU period have the same value NIW *KE* as the forward simulations.

296 **5. Summary and discussion**

297 The primary purpose of this paper is to investigate the spurious high frequency waves generated
298 by the NCODA DA procedure in the Navy's ocean forecast system. Using the analysis presented
299 here, we show that the current implementation of DA in HYCOM introduces spurious NIWs that
300 can overshadow the generation and propagation of the physical internal waves in the model. These
301 spurious waves contaminate the short-range forecast that provides the background state for the next
302 analysis, adding to the difficulty of extracting useful information from the observation data (Our-
303 mieres et al., 2006). Although this may have little impact on the large-scale mesoscale circulation,
304 it does affect small-scale/high-frequency ocean dynamics, especially in high-resolution simulations
305 that do resolve these scales. Our main conclusions from this study are:

- 306 1. The current implementation of data assimilation in the US Navy's operational global ocean
307 prediction system generates spurious NIWs during updates.
- 308 2. The spurious NIWs mostly project on low baroclinic modes that propagate long horizontal
309 distances from their generation sites. The presence of these spurious waves makes the model
310 simulations very difficult to use for the study of small-scale/high-frequency motions.
- 311 3. The generation of spurious NIWs can be minimized by increasing the duration of IAU period
312 to 24 hours.

313 The past studies on the impact of DA induced model adjustments and their consequences have
314 mainly focused only on the accuracy of mesoscale eddies in the forecast fields, and not explicitly on

315 the quality of the fields in terms of high-frequency/small-scale motions. Bell et al. (2004) discuss
316 how the incorporation of thermal data into an ocean model near the equator frequently leads to a
317 dynamically unbalanced state with unrealistic deep overturning circulations in the equatorial region.
318 More recently, Pilo et al. (2018) discuss the impact of DA on vertical velocities (chosen because of
319 their sensitivity to model dynamic balances) within mesoscale eddies in the subtropics. They find
320 that the model adjustment following the insertion of increments distorts the eddies on the first day
321 after assimilation, and suggest that the model fields from the first day after assimilation should be
322 disregarded. However, our study shows that the low-mode NIWs generated as a consequence of
323 the DA induced model adjustment are persistent and propagate long distances from their generation
324 sites. These spurious NIWs are capable of disrupting the high-frequency dynamics in short-medium
325 range forecasts.

326 The importance of accurate representation of internal wave dynamics in the global ocean models
327 has been widely reported in the past (e.g., Arbic et al., 2010; Simmons & Alford, 2012; Buijsman
328 et al., 2020; Raja et al., 2022; Arbic et al., 2022). Recently, as the spatial resolution of the ocean
329 forecast systems increases, the need for simulations of global ocean models that simultaneously
330 include realistic atmospheric and tidal forcing have grown (Arbic, 2022). The prediction of internal
331 tide amplitude and phase (especially that of the non-phase-locked internal tides) require accurate
332 forecasts of the mesoscale eddies and time-varying stratification (Shriver et al., 2012; Luecke et al.,
333 2020). This demand for assimilative simulations that can represent internal tides well will likely
334 increase further as the next generation altimeter missions with fine spatial resolutions such as the
335 Surface Water Ocean Topography (SWOT) mission come online and require accurate corrections of
336 the high-frequency internal wave motions.

337 Moreover, global ocean models with DA such as operational HYCOM, are often used for the
338 initialization of various regional models (Prasad & Hogan, 2007; Barth et al., 2008). These nested
339 regional models with very high spatial resolutions are used for studying ocean processes of short
340 length and time scales because the global HYCOM does not sufficiently resolve such detailed
341 physics due to its coarser grid resolution. The remotely generated internal waves can affect the
342 energetics in the regional simulations as they propagate into the nested domain and dissipate there

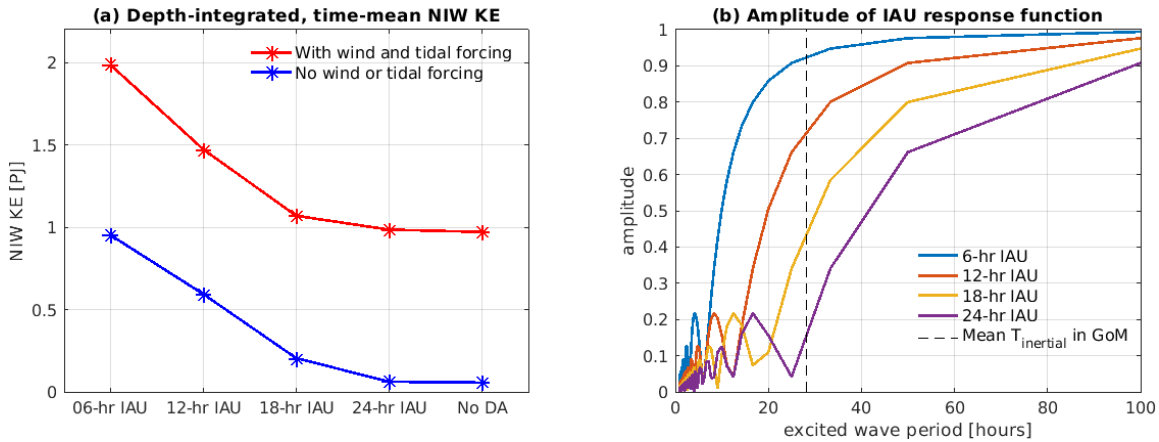


Figure 9: (a) Depth-integrated, time-mean NIW kinetic energy in the Gulf of Mexico regional simulations with IAU periods of 6, 12, 18 and 24 hours. (b) The amplitude of the IAU response function (calculated according to Bloom et al. (1996)) for the same IAU periods with respect to the excited wave periods. The black dashed line shows the mean inertial period in the Gulf of Mexico.

343 (Nelson et al., 2020; Siyanbola et al., 2023). Hence, it is crucial to improve the representation of
 344 internal waves in assimilative ocean model simulations.

345 The IAU method introduced by Bloom et al. (1996) was originally developed as an initialization
 346 procedure for three-dimensional atmospheric DA systems. The IAU has since been incorporated
 347 into ocean forecast systems that use intermittent DA methods, and has found some notable success
 348 in minimizing the initialization shocks during updates (Ourmières et al., 2006). The IAU process
 349 incorporates analysis increments, calculated by the DA system, into a model in a gradual manner
 350 by using the increments as constant forcings in the model’s prognostic equations over a period of
 351 time, i.e. the IAU period, centered on an analysis time. However, the method has not been tested
 352 enough to check if it really prevents horizontally propagating spurious NIWs in the model output
 353 fields. We show that the 3-hr IAU period used in the Navy’s ocean forecast systems (GOFS 3.5, and
 354 the soon-to-be operational ESPC) does not prevent the generation of spurious NIWs in the analysis
 355 fields.

356 In our analyses, we demonstrate that the generation of spurious NIWs during DA can be mini-
 357 mized by using a longer IAU period than the typical 3-hour IAU used in the ESPC system. Without

358 wind and tidal forcing (blue line in Figure 9a), when the IAU period is 6 hours, the spurious near-
359 inertial energy is as much as the near-inertial energy in the forward simulation with wind and tidal
360 forcing (red line Figure 9a). Increasing the IAU period decreases the spurious NIW energy, and
361 with a 24-hr IAU period, we find that the assimilative simulations have the same NIW energy as the
362 forward simulation (implying that all the spurious waves are removed with the 24-hr IAU).

363 While introducing the IAU technique, Bloom et al. (1996) compare various approaches of in-
364 troducing the analysis increment into a linear oscillator with complex frequency. They compare the
365 IAU method with direct insertion of the analysis and demonstrate that, in contrast to direct insertion,
366 which has an amplitude that is independent of frequency, IAU causes a neutral oscillator's reaction
367 to the insertion to have a diminishing amplitude with rising frequency. In other words, the IAU pro-
368 cess acts as a low-pass filter on the analysis fields that diminishes the DA-generated high-frequency
369 motions, especially those with time periods less than the IAU period. In Figure 9b, we show the
370 amplitude of the IAU response function, calculated according to Bloom et al. (1996), for the differ-
371 ent IAU periods we tested in our experiments. The spurious motions that are forced by the insertion
372 of increments with wave periods shorter than the IAU period are diminished.

373 Our analyses in the context of Bloom et al. (1996) imply that the duration of the IAU period
374 should be longer than the local inertial period, in order to effectively minimize the generation of
375 spurious NIWs. This is not practically possible to implement since the inertial period increases to
376 infinity as the latitude decreases in the global ocean. However, from the global map of spurious NIW
377 kinetic energy (Figure 5c), we see that the spurious NIWs are excited mostly in the mid-latitudes.
378 Therefore, increasing the IAU period to 24 hours will diminish the generation of spurious NIWs in
379 most of the ocean (poleward of $\sim 30^\circ$). We will test this hypothesis using a global HYCOM simula-
380 tion with 24-hour IAU period in a future paper. In this future paper, we will also investigate whether
381 increasing the duration of the IAU period to optimize for minimum spurious wave generation affect
382 the forecast quality in terms of large-scale flows.

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